

## UNIT - III

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### Maxwell's Equations.

1. Introduction to Time varying fields.
2. Faraday's law.
3. Continuity Equation.
4. Inconsistency of Ampere's law.
5. Displacement Current Density
  - a) Displacement current.
  - b) Conduction current.  $\xrightarrow{q}$  Relaxation time
6. Maxwell's Equations for Time varying fields.
7. Boundary conditions.
8. Problems.

MAXWELL'S EQUATIONS

- The electrostatic fields are usually produced by static electric charges, whereas magnetostatic fields are due to motion of electric charges with uniform velocity (direct current) (or) static magnetic charges.
- The time-varying fields are (or) waves are usually due to accelerated charges (or) time-varying currents.
  - \* stationary charges → Electrostatic fields.
  - \* Steady currents → Magnetostatic fields.
  - \* Time-varying currents → Electromagnetic fields (or) waves.
- The relationship between time varying electric and magnetic fields are known as Maxwell's equations.

Faraday's Law :

Faraday's law states that the induced electromotive force (emf) (or)  $V_{emf}$  in any closed circuit is equal to the rate of change of magnetic flux linkage ( $\lambda$ ) by the circuit.

(or)

It states that in a magnetic field, if the conductor is in motion (or) if the field is time varying then the induced emf in a closed circuit is equal to the time rate of change of magnetic flux linkage by the circuit.

- It can be expressed as

$$V_{emf} = -\frac{d\lambda}{dt} = -\frac{d}{dt}(N\psi) \quad \therefore \lambda = N\psi$$

$$\therefore V_{emf} = -N \frac{d\psi}{dt} \text{ Volts.}$$

- The negative sign indicates that the induced emf and flux are in opposite direction is called Lenz's law.

- The e.m.f is nothing but a voltage that induces from changing magnetic fields (or) motion of conductors in a magnetic field
- There are three conditions for the induced emf.
  1. Transformer emf (or) stationary loop in time-varying B field.
  2. Generator emf (or) motional emf (or) moving loop in static B field.
  3. Both Transformer & generator emf (or) moving loop in Time varying field.

### ① Transformer emf :

- Consider a transformer (stationary ckt) as shown in fig.
- When a time-varying current is applied, it produces a time varying magnetic flux in the primary coil, that induces an emf in the secondary coil. This emf is called Transformer emf  
 (or) statically induced emf.

→ According to Faraday's law, (for  $N=1$ )

$$V = - \frac{d\psi}{dt}$$

→ But we know that  $\psi = \int_S B \cdot dS$  and  $V = \oint_L E \cdot dl$

$$\text{then } \oint_L E \cdot dl = - \frac{d}{dt} \int_S B \cdot dS$$

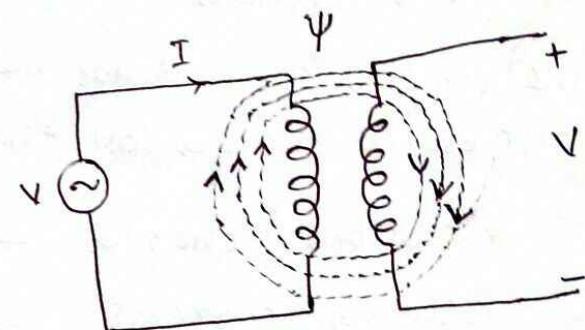
→ Using Stokes theorem on LHS side

$$\int_S (\nabla \times E) \cdot dS = - \int_S \frac{dB}{dt} \cdot dS$$

→ Removing surface integrals on both sides, then

$$\boxed{\nabla \times E = - \frac{\partial B}{\partial t}}$$

- This is one of the Maxwell's equation for time varying fields. It shows that time-varying E field is not conservative ( $\nabla \times E \neq 0$ ).
- If the flux density is constant for static field, then the field is conservative i.e.,  $\nabla \times E = 0$  and  $\oint_L E \cdot dl = 0$ .



## Equation of Continuity for time varying fields :

- When the current is flowing through a conductor due to conservation of charge, the total current flowing out from a volume must be equal to the rate of decrease of charge within the volume.
- The sum of divergence of current density ( $J$ ) and rate of change in volume charge density ( $\rho_v$ ) is equal to zero is called continuity equation (or) equation of continuity for time varying fields.

$$\nabla \cdot J + \frac{\partial \rho_v}{\partial t} = 0$$

Proof:

We know that current through the closed surface is

$$I = \oint_S J \cdot dS$$

Apply divergence theorem

$$I = \int_{Vol} (\nabla \cdot J) dV \rightarrow (1)$$

→ Current flow with in the closed surface is

$$I = - \frac{dQ}{dt}$$

$$I = - \frac{d}{dt} \left[ \int_{Vol} \rho_v dV \right]$$

$$I = \int_{Vol} - \frac{\partial \rho_v}{\partial t} \cdot dV \rightarrow (2)$$

→ Equating eq(1) & (2)

$$\int_{Vol} (\nabla \cdot J) dV = \int_{Vol} - \frac{\partial \rho_v}{\partial t} dV$$

Removing volume integrals on both sides

$$\nabla \cdot J = - \frac{\partial \rho_v}{\partial t}$$

$\Rightarrow$

$$\nabla \cdot J + \frac{\partial \rho_v}{\partial t} = 0$$

$$\begin{aligned} J &= \frac{dI}{dS} \\ dI &= J \cdot dS \\ I &= \int_S J \cdot dS \end{aligned}$$

$$\begin{aligned} \rho_v &= \frac{dQ}{dV} \\ dQ &= \rho_v dV \\ Q &= \int V \rho_v dV \end{aligned}$$

## Inconsistency of Ampere's law :

→ From the definition of ampere's circuit law

$$\oint \mathbf{H} \cdot d\mathbf{l} = I$$

Apply stokes theorem on L.H.S. side

$$\int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S} = I$$

$$\therefore I = \int_S \mathbf{J} \cdot d\mathbf{S}$$

$$\int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S} = \int_S \mathbf{J} \cdot d\mathbf{S}$$

Removing surface integrals on both sides

$$\boxed{\nabla \times \mathbf{H} = \mathbf{J}}$$

Apply divergence operation

$$\nabla \cdot (\nabla \times \mathbf{H}) = \nabla \cdot \mathbf{J}$$

→ The divergence of the curl of any vector field is identically zero.

Hence

$$0 = \nabla \cdot \mathbf{J}$$

$$\therefore \nabla \cdot (\nabla \times \mathbf{H}) = 0$$

$$\boxed{\therefore \nabla \cdot \mathbf{J} = 0}$$

$$\boxed{\nabla \cdot \mathbf{J} = - \frac{\partial \rho_e}{\partial t} \neq 0}$$

→ from continuity equation

If  $\boxed{\nabla \cdot \mathbf{J} = 0}$  then  $\boxed{\frac{\partial \rho_e}{\partial t} = 0}$

→ The above quantity cannot be zero. That means

$$\int \mathbf{H} \cdot d\mathbf{l} = I \quad (1) \quad \nabla \times \mathbf{H} = \mathbf{J} \quad \text{are not compatible}$$

for time-varying conditions.

→ therefore ampere's circuit law is inconsistent.

## Displacement Current Density :

- We know that the amperes law  $\oint H \cdot dl = I$  (8) Maxwell's equation  $\nabla \times H = J$  are not compatible for time-varying conditions.
- therefore some modification is required for maxwell's equation.  $\nabla \times H = J$ . Replace current density  $J$  with  $J + J_d$ . where  $J_d$  is the displacement current density &  $J$  conduction current density.

$$\therefore \nabla \times H = J + J_d \quad \rightarrow (1)$$

Apply divergence operation

$$\nabla \cdot (\nabla \times H) = \nabla \cdot (J + J_d)$$

$$0 = \nabla \cdot J + \nabla \cdot J_d$$

$$\therefore \nabla \cdot J_d = -\nabla \cdot J$$

$$\nabla \cdot J_d = \frac{\partial \rho_e}{\partial t}$$

$$\therefore \text{continuity eq } \nabla \cdot J = -\frac{\partial \rho_e}{\partial t}$$

$$\nabla \cdot J_d = \frac{\partial}{\partial t} (\nabla \cdot D)$$

$$\therefore \text{gauss's law } \nabla \cdot D = \rho_e$$

$$\nabla \cdot J_d = \nabla \cdot \frac{\partial D}{\partial t}$$

$$\boxed{\therefore J_d = \frac{\partial D}{\partial t}}$$

∴ Rate of change of electric flux density  $D$  is called displacement current density ( $J_d$ ).

$$\rightarrow \text{from eq (1)} \quad \nabla \times H = J + J_d \Rightarrow \boxed{\nabla \times H = J + \frac{\partial D}{\partial t}}$$

→ This is the maxwell's equation based on Amperes circuit law for time-varying field.

## Displacement Current :

- The current flow due to time-varying electric field is called displacement current. (B) The current flow <sup>through</sup> dielectric material is called displacement current.
- It is denoted with  $I_D$  and can be computed from displacement current density

$$I_D = \oint_S J_D \cdot d\vec{S}$$

where  $J_D = \frac{\partial D}{\partial t}$

## Conduction current :

- The current flow through the conductor (B) conducting material is called conduction current
- It is denoted with  $I_a$  and can be computed from conduction current density.

$$I_a = \oint_S J \cdot d\vec{S}$$

where  $J = \sigma E$ .

Problem 9.4 A parallel plate capacitor with plate area of  $5 \text{ cm}^2$  and plate separation of  $3 \text{ mm}$  has a voltage  $50 \sin 10^3 t \text{ V}$  applied to its plates. Calculate the displacement current assuming  $\epsilon = 2\epsilon_0$ .

Sol plate area  $S = 5 \text{ cm}^2 = 5 \times 10^{-4} \text{ m}^2$  | voltage  $V = 50 \sin 10^3 t \text{ V}$   
plate separation  $d = 3 \text{ mm} = 3 \times 10^{-3} \text{ m}$  |  $\epsilon = 2\epsilon_0$ .

$$I_D = \oint_S J_D \cdot d\vec{S} = J_D \cdot S = S \cdot \frac{\partial D}{\partial t}$$

$$\therefore J_D = \frac{\partial D}{\partial t}$$

$$I_D = S \cdot \frac{d}{dt} (\epsilon E) = S \epsilon \frac{d(E)}{dt} = S \epsilon \frac{d}{dt} \left( \frac{V}{d} \right)$$

$$D = \epsilon E$$

$$E = \frac{V}{d}$$

$$I_D = \frac{S \epsilon}{d} \cdot \frac{dV}{dt} = \frac{5 \times 10^{-4} \times 2\epsilon_0}{3 \times 10^{-3}} \cdot \frac{d}{dt} (50 \sin 10^3 t)$$

$$I_D = \frac{5 \times 10^{-4} \times 2}{10^9 \times 36\pi \times 3 \times 10^{-3}} 50 \cos(10^3 t) \times 10^3 = 147.4 \cos 10^3 t \text{ nA}$$

$\therefore I_D = 147.4 \cos 10^3 t \text{ nA}$

## Relaxation Time :

It is the time taken by the point charge when placed in a interior of the conductor drops to  $e^{-1}$  ( $= 36.8\%$ ) percent of its initial value.

→ Consider point form of ohm's law (8) I.N.K.T  $J = \sigma E$

→ from continuity Equation  $\nabla \cdot J = - \frac{\partial P_V}{\partial t}$ .

$$\nabla \cdot (\sigma E) = - \frac{\partial P_V}{\partial t} \Rightarrow \sigma (\nabla \cdot E) = - \frac{\partial P_V}{\partial t}$$

$$\sigma (\nabla \cdot \frac{D}{\epsilon_0}) = - \frac{\partial P_V}{\partial t} \Rightarrow \frac{\sigma}{\epsilon_0} (\nabla \cdot D) = - \frac{\partial P_V}{\partial t}$$

$$\frac{\sigma}{\epsilon_0} (P_V) = - \frac{\partial P_V}{\partial t} \Rightarrow \frac{\sigma}{\epsilon_0} dt = - \frac{\partial P_V}{P_V}$$

$$-\frac{\sigma}{\epsilon_0} dt = \frac{\partial P_V}{P_V}$$

$$-\frac{\sigma}{\epsilon_0} t + C = \ln P_V$$

$$\left| \begin{array}{l} \frac{1}{x} dx = \ln x \\ C = \ln P_{V0} \end{array} \right.$$

$$-\frac{\sigma}{\epsilon_0} t = \ln P_V - \ln P_{V0}$$

$$-\frac{\sigma}{\epsilon_0} t = \ln \left( \frac{P_V}{P_{V0}} \right)$$

$$\frac{P_V}{P_{V0}} = e^{-\frac{\sigma}{\epsilon_0} t}$$

$$\boxed{P_V = P_{V0} e^{-\frac{\sigma}{\epsilon_0} t} = P_{V0} e^{-t/\tau}} \quad \therefore \tau = \frac{\epsilon_0}{\sigma}$$

This expression shows that the volume charge density exponentially decays with time constant.

→ At  $t=0$  ;  $P_V = P_{V0}$

→ At  $t = \frac{\epsilon_0}{\sigma}$  ;  $P_V = P_{V0} e^{-1} = 37\% \text{ of } P_{V0}$

## Maxwell's Equations for time varying Fields :

We know that the stationary charges produces electrostatic fields, steady current produces magneto static fields and the time-varying current produces electromagnetic fields E, D, H and B.  
 → Maxwell's equations are the relations among the electric field-intensity E, electric flux density D, magnetic field intensity H and magnetic flux density B.

$$(1) \quad \nabla \cdot D = \rho_v$$

$$(2) \quad \nabla \cdot B = 0$$

$$(3) \quad \nabla \times E = -\frac{\partial B}{\partial t}$$

$$(4) \quad \nabla \times H = I + \frac{\partial D}{\partial t}.$$

### Equation 1 :

Divergence of electric flux density is equal to the volume charge density  $\rho_v$

$$\boxed{\nabla \cdot D = \rho_v}$$

Proof:

from the definition of Gauss's law

$$\Psi = Q = \oint_S D \cdot dS$$

Apply divergence theorem

$$Q = \int_{Vol} (\nabla \cdot D) dV \rightarrow (1)$$

The charge enclosed by the volume  $\Psi$

$$Q = \int_{Vol} \rho_v dV \rightarrow (2)$$

Equating eq (1) & (2)

$$\boxed{\int_{Vol} (\nabla \cdot D) dV = \int_{Vol} \rho_v dV} \rightarrow \text{It is integral form}$$

Removing volume integrals on both sides

$$\boxed{\nabla \cdot D = \rho_v} \rightarrow \text{It is point form (or) differential form.}$$

### Equation 2 :

Divergence of magnetic flux density  $B$  around a closed loop is zero.

$$\boxed{\nabla \cdot B = 0}$$

Proof: The total flux through any closed surface will in the magnetic field  $B$  is zero

$$\Psi = 0$$

$$\boxed{\int_S B \cdot dS = 0}$$

→ It is integral form

$$\left| \therefore \Psi = \int_S B \cdot dS \right.$$

Apply divergence theorem

$$\int_{\text{vol}} (\nabla \cdot B) dv = 0$$

$$\boxed{\nabla \cdot B = 0}$$

→ It is point form (or) differential form.

### Equation 3 :

Curl of a electric field intensity  $E$  is equal to the rate of decrease in magnetic flux density  $B$ .

$$\boxed{\nabla \times E = -\frac{\partial B}{\partial t}}$$

Proof: from faradays law of electromagnetic induction.

$$V_{\text{emf}} = -\frac{d\lambda}{dt} = -\frac{d}{dt} N\Psi$$

$$\left| \therefore \lambda = N\Psi \right. \\ V_{\text{emf}} = -V = \oint_L E \cdot dl$$

$$V_{\text{emf}} = -N \frac{d\Psi}{dt} = -\frac{d\Psi}{dt} \quad (\text{For } N=1)$$

But we know that  $V_{\text{emf}} = \oint_L E \cdot dl$  and  $\Psi = \int_S B \cdot dS$

then  $\oint_L E \cdot dl = -\frac{d}{dt} \int_S B \cdot dS$

Apply stokes theorem to the LHS

$$\oint (\nabla \times E) \cdot dS = - \int \frac{dB}{dt} \cdot dS$$

Removing Surface integrals on both sides

$$\boxed{\nabla \times E = - \frac{\partial B}{\partial t}} \rightarrow \text{It is Point form (or) differential form.}$$

$$\boxed{\oint L E \cdot dL = - \int_S \frac{\partial B}{\partial t} \cdot dS} \rightarrow \text{It is Integral form.}$$

Equation 4 :

Curl of magnetic field intensity  $H$  is equal to the sum of conduction and displacement current densities.

$$\boxed{\nabla \times H = J + \frac{\partial D}{\partial t}}$$

Proof : We know that the amperes law  $\oint L H \cdot dL = I$  and maxwell's equation  $\nabla \times H = J$  are not compatible for time varying conditions.

→ therefore some modification is required for maxwell's equation  $\nabla \times H = J$   
Replace current density  $J$  with  $J + JD$

$$\nabla \times H = J + JD \longrightarrow (1)$$

Apply divergence operation

$$\nabla \cdot (\nabla \times H) = \nabla \cdot (J + JD)$$

$$0 = \nabla \cdot J + \nabla \cdot JD$$

$$\therefore \nabla \cdot JD = - \nabla \cdot J = \frac{\partial \rho_V}{\partial t} = \frac{\partial}{\partial t} (\nabla \cdot D)$$

$$\nabla \cdot JD = \nabla \cdot \frac{\partial D}{\partial t}$$

$$JD = \frac{\partial D}{\partial t}$$

$$\therefore \text{from eq(1)} \quad \boxed{\nabla \times H = J + \frac{\partial D}{\partial t}} \rightarrow \text{It is Point form (or) differential form}$$

Continuity eq

$$\nabla \cdot J = - \frac{d \rho_V}{dt}$$

Gauss law

$$\nabla \cdot D = \rho_V$$

$$\boxed{\oint L H \cdot dL = \int_S (J + \frac{\partial D}{\partial t}) \cdot dS} \rightarrow \text{It is Integral form.}$$

## Maxwell's equations in final forms :

<u>Point (differential) form</u>	<u>Integral form</u>	<u>Remarks</u>
(1) $\nabla \cdot D = \rho_v$	$\oint_S D \cdot dS = \int_{Vol} \rho_v dv$	Gauss's law for electrostatic field
(2) $\nabla \cdot B = 0$	$\oint_S B \cdot dS = 0$	Gauss's law for magnetostatic field
(3) $\nabla \times E = -\frac{\partial B}{\partial t}$	$\oint_L E \cdot dl = - \int_S \frac{\partial B}{\partial t} \cdot dS$	Faraday's law
(4) $\nabla \times H = J + \frac{\partial D}{\partial t}$	$\oint_L H \cdot dl = \int_S \left( J + \frac{\partial D}{\partial t} \right) \cdot dS$	Ampere's circuit law.

Maxwell's equations for free space : ( $\sigma=0$ ,  $J=0$  &  $\rho_v=0$ ).

<u>Point (a) Differential form</u>	<u>Integral form</u>
(1) $\nabla \cdot D = 0$	$\oint_S D \cdot dS = 0$
(2) $\nabla \cdot B = 0$	$\oint_S B \cdot dS = 0$
(3) $\nabla \times E = -\frac{\partial B}{\partial t}$	$\oint_L E \cdot dl = \int_S \frac{\partial B}{\partial t} \cdot dS$
(4) $\nabla \times H = \frac{\partial D}{\partial t}$	$\oint_L H \cdot dl = \int_S \frac{\partial D}{\partial t} \cdot dS$

Practise Ex  
Q.4In free space,  $E = 20 \cos(\omega t - 50x) \text{ ay v/m}$ calculate a)  $J_d$  b)  $H$  c)  $\omega$ .

SOL

In free space  $\sigma = 0$ ;  $J = \sigma E = 0$  and  $P_E = 0$ .

$$\epsilon = \epsilon_0 \text{ and } \mu = \mu_0$$

Given  $E = 20 \cos(\omega t - 50x) \text{ ay v/m}$ .a) Displacement current density ( $J_d$ ):

$$J_d = \frac{dD}{dt} = \frac{d(\epsilon_0 E)}{dt} = \epsilon_0 \frac{dE}{dt}$$

$$J_d = \epsilon_0 \frac{d}{dt}(20 \cos(\omega t - 50x) \text{ ay})$$

$$J_d = \epsilon_0 20 [-\sin(\omega t - 50x) \text{ ay}] \cdot \omega$$

$$J_d = -20 \omega \epsilon_0 \sin(\omega t - 50x) \text{ ay Amp/m}^2$$

b) Magnetic field Intensity ( $H$ ):from Maxwell's 3rd equation  $\nabla \times E = -\frac{\partial B}{\partial t}$ 

$$\text{then } \frac{dB}{dt} = -\nabla \times E$$

$$\nabla \times E = \begin{vmatrix} \text{ax} & \text{ay} & \text{az} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & 20 \cos(\omega t - 50x) & 0 \end{vmatrix}$$

$$\nabla \times E = \text{ax} \left[ 0 - \frac{\partial}{\partial z} (20 \cos(\omega t - 50x)) \right] - \text{ay} [0 - 0] + \text{az} \left[ \frac{\partial}{\partial x} (20 \cos(\omega t - 50x)) - 0 \right]$$

$$\nabla \times E = \text{ax}(0) - \text{ay}(0) + \text{az} \left[ -20 \sin(\omega t - 50x) \cdot (-50) \right]$$

$$\nabla \times E = 1000 \sin(\omega t - 50x) \text{ az.}$$

$$\frac{dB}{dt} = -\nabla \times E = -1000 \sin(\omega t - 50x) \text{ az}$$

Integrate on both sides w.r.t  $t$

$$\text{then } B = -1000 \int \sin(\omega t - 50x) dz \cdot dt$$

$$B = (-1000) \frac{-\cos(\omega t - 50x) az}{\omega} = \frac{1000 \cos(\omega t - 50x) az}{\omega}$$

$$\text{But we know that } B = \mu_0 H \Rightarrow H = \frac{B}{\mu_0}$$

$$\text{then } H = \frac{1000 \cos(\omega t - 50x) az}{\omega \mu_0}$$

c) frequency ( $\omega$ ):

$$\text{from 4th Maxwell's equation } \nabla \times H = J + J_d = J_d$$

$$\because J = 0$$

$$\nabla \times H = \begin{vmatrix} ax & ay & az \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & 0 & \frac{1000 \cos(\omega t - 50x)}{\omega \mu_0} \end{vmatrix}$$

$$\nabla \times H = ax \left[ \frac{\partial}{\partial y} \left( \frac{1000}{\omega \mu_0} \cos(\omega t - 50x) - 0 \right) - ay \left[ \frac{\partial}{\partial x} \left( \frac{1000}{\omega \mu_0} \cos(\omega t - 50x) - 0 \right) \right] + az [0 - 0] \right]$$

$$\nabla \times H = ax [0] - ay \left[ \frac{1000}{\omega \mu_0} (-\sin(\omega t - 50x)) \cdot (-50) \right] + az [0]$$

$$\nabla \times H = - \frac{50000}{\omega \mu_0} \sin(\omega t - 50x) ay$$

$$\text{But we know that in free space } \nabla \times H = J_d$$

$$\text{ie } - \frac{50000}{\omega \mu_0} \sin(\omega t - 50x) ay = -20\pi \epsilon_0 \sin(\omega t - 50x) ay$$

$$\frac{50000}{\omega \mu_0} = 20\pi \omega \epsilon_0$$

$$\omega^2 = \frac{2500}{\mu_0 \epsilon_0} = \frac{2500 \times 10^9 \times 36\pi}{4\pi \times 10^{-7}}$$

$$\epsilon_0 = \frac{1}{10^9 \times 36\pi}$$

$$\mu_0 = 4\pi \times 10^{-7}$$

$$\omega^2 = 2500 \times 9 \times 10^9 \times 10^7$$

$$\omega^2 = 22500 \times 10^{16}$$

$$\omega = \sqrt{22500 \times 10^{16}}$$

$$\omega = 150 \times 10^8 \text{ rad/sec}$$

$$\boxed{\omega = 1.5 \times 10^{10} \text{ rad/sec}}$$

Problem  
T-8

ME-7

In medium characterised by  $\sigma = 0$ ,  $\mu = \mu_0$ ,  $\epsilon = \epsilon_0$  and

$$E = 20 \sin(10^8 t - \beta z) \text{ ay} \text{ v/m}$$
 calculate a)  $\beta$  and b)  $H$ .

Sol

Given  $E = 20 \sin(10^8 t - \beta z) \text{ ay} \text{ v/m}$

from Maxwell's 3rd equation

$$\nabla \times E = -\frac{d\beta}{dt} \rightarrow (1)$$

$$\therefore \nabla \times E = \begin{vmatrix} ax & ay & az \\ \frac{d}{dx} & \frac{d}{dy} & \frac{d}{dz} \\ 0 & 20 \sin(10^8 t - \beta z) & 0 \end{vmatrix} = ax \left[ 0 - \frac{d}{dz} (20 \sin(10^8 t - \beta z)) \right] - ay [0 - 0] + az \left[ \frac{d}{dx} (20 \sin(10^8 t - \beta z)) - 0 \right]$$

$$\nabla \times E = -ax [20 \cos(10^8 t - \beta z) (-\beta)] - ay [0] + az [0]$$

$$\nabla \times E = +20\beta \cos(10^8 t - \beta z) ax$$

from (1)  $\nabla \times E = -\frac{d}{dt}(\mu_0 H) = -\mu_0 \frac{d}{dt}(H) \Rightarrow \frac{d(H)}{dt} = -\frac{1}{\mu_0} (\nabla \times E)$

$$H = -\frac{1}{\mu_0} \int (\nabla \times E) dt$$

$$\therefore H = -\frac{1}{\mu_0} \int +20\beta \cos(10^8 t - \beta z) ax dt$$

$$H = -\frac{20\beta}{\mu_0} \frac{\sin(10^8 t - \beta z) ax}{10^8} = -\frac{20\beta}{\mu_0 \cdot 10^8} \sin(10^8 t - \beta z) ax$$

$$\nabla \times H = \begin{vmatrix} ax & ay & az \\ \frac{d}{dx} & \frac{d}{dy} & \frac{d}{dz} \\ -\frac{20\beta}{\mu_0 \cdot 10^8} \sin(10^8 t - \beta z) & 0 & 0 \end{vmatrix} = ax [0 - 0] - ay \left[ 0 - \frac{d}{dz} \left( -\frac{20\beta}{10^8 \mu_0} \sin(10^8 t - \beta z) \right) \right] + az \left[ 0 - \frac{d}{dy} \left( -\frac{20\beta}{10^8 \mu_0} \sin(10^8 t - \beta z) \right) \right]$$

$$\nabla \times H = ax [0] - ay \left[ \frac{20\beta}{10^8 \mu_0} \cos(10^8 t - \beta z) (-\beta) \right] + az [0]$$

$$\nabla \times H = \frac{20\beta^2}{10^8 \mu_0} \cos(10^8 t - \beta z) ay$$

$$\nabla \times H = J + JD \quad \text{If } \sigma = 0 \text{ then } J = \sigma E = 0$$

$$\nabla \times H = J_d = \frac{dD}{dt} = \epsilon_0 \frac{\partial E}{\partial t} \Rightarrow \frac{\partial E}{\partial t} = \frac{1}{\epsilon_0} \nabla \times H$$

$$\Rightarrow E = \frac{1}{\epsilon_0} \int (\nabla \times H) dt$$

$$\therefore E = \frac{1}{\epsilon_0} \int \frac{20\beta^2}{10^8 \mu_0} \cos(10^8 t - \beta z) ay dt$$

$$E = \frac{20\beta^2}{10^8 \mu_0 \epsilon_0} \frac{\sin(10^8 t - \beta z) ay}{10^8} = \frac{20\beta^2}{10^{16} \mu_0 \epsilon_0} \sin(10^8 t - \beta z) ay$$

Now Comparing this E with given E

$$\frac{20\beta^2}{10^{16} \mu_0 \epsilon_0} \sin(10^8 t - \beta z) ay = 20 \sin(10^8 t - \beta z) ay$$

$$\beta^2 = 10^{16} \mu_0 \epsilon_0 \Rightarrow \beta = 10^8 \sqrt{\mu_0 \epsilon_0} = 10^8 \sqrt{\frac{4\pi \times 10^{-7}}{36\pi \times 10^{-9}}}$$

$$\beta = 10^8 \sqrt{\frac{10^{16}}{9}} = 10^8 \times 10^8 \times \frac{1}{3} = \frac{1}{3} = 0.33$$

$$\therefore \beta = \pm 0.33 \quad (3)$$

$$\text{then } H = \frac{-1}{6\pi} \sin(10^8 t - \frac{1}{3}z) ax \quad \text{for } \beta = +\frac{1}{3}$$

$$H = \frac{1}{6\pi} \sin(10^8 t + \frac{1}{3}z) ax \quad \text{for } \beta = -\frac{1}{3}$$

Problem Ex  
9.8

A medium is characterised by  $\sigma=0$ ,  $\mu=2\mu_0$  and  $E=5\epsilon_0$

If  $H = 2 \cos(\omega t - 3y) az$  A/m. Calculate a) w and b) E

Sol From Maxwell's 4<sup>th</sup> equation  $\nabla \times H = J + J_d = 0 + \frac{dD}{dt}$

$$\nabla \times H = \frac{dE}{dt} = \epsilon \frac{dE}{dt} \Rightarrow \frac{dE}{dt} = \frac{1}{\epsilon} \nabla \times H$$

$$\Rightarrow E = \frac{1}{5\epsilon_0} \int \nabla \times H \cdot dt \rightarrow (1)$$

$$\nabla \times H = \begin{vmatrix} ax & ay & az \\ \frac{d}{dx} & \frac{d}{dy} & \frac{d}{dz} \\ 0 & 0 & 2 \cos(\omega t - 3y) \end{vmatrix} = ax \left[ \frac{d}{dy} (2 \cos(\omega t - 3y)) - 0 \right] - ay [0 - 0] + az [0 - 0]$$

$$= 2 (-\sin(\omega t - 3y)) (-3) ax$$

$$\nabla \times H = 6 \sin(\omega t - 3y) ax$$

from eq(1)

$$E = \frac{1}{5\epsilon_0} \int (\nabla \times H) dt = \frac{1}{5\epsilon_0} \int 6 \sin(\omega t - 3y) ax$$

$$E = \frac{6}{5\epsilon_0} \left( -\frac{\cos(\omega t - 3y)}{\omega} ax \right) = -\frac{6}{5\omega\epsilon_0} \cos(\omega t - 3y) ax \rightarrow (2)$$

from maxwell's 3rd equation

$$\nabla \times E = -\frac{\partial B}{\partial t} = -\frac{\partial \mu H}{\partial t} = -\mu \frac{d(H)}{dt}$$

$$\Rightarrow \frac{d(H)}{dt} = -\frac{1}{\mu} \nabla \times E \Rightarrow H = -\frac{1}{2\mu_0} \int (\nabla \times E) dt \rightarrow (3)$$

$$\nabla \times E = \begin{vmatrix} ax & ay & az \\ \frac{d}{dx} & \frac{d}{dy} & \frac{d}{dz} \\ -\frac{6}{5\omega\epsilon_0} \cos(\omega t - 3y) & 0 & 0 \end{vmatrix} = ax[0-0] - ay[0-0] + az[0 - \frac{d}{dy} \left( -\frac{6}{5\omega\epsilon_0} \cos(\omega t - 3y) \right)]$$

$$\nabla \times E = ax(0) - ay(0) + az \left[ \frac{6}{5\omega\epsilon_0} [-\sin(\omega t - 3y) (-3)] \right]$$

$$\nabla \times E = \frac{18}{5\omega\epsilon_0} \sin(\omega t - 3y) az$$

$$\text{from eq(3)} \quad H = \frac{-1}{2\mu_0} \int \frac{18}{5\omega\epsilon_0} \sin(\omega t - 3y) az dt$$

$$H = \frac{-18}{10\omega\epsilon_0\mu_0} \frac{-\cos(\omega t - 3y) az}{\omega} = \frac{18}{10\omega^2\epsilon_0\mu_0} \cos(\omega t - 3y) az$$

Now compare this H with given H

$$\frac{18}{10\omega^2\epsilon_0\mu_0} \cos(\omega t - 3y) az = 2 \cos(\omega t - 3y) az$$

$$\omega^2 = \frac{9}{10\epsilon_0\mu_0} = \frac{9 \times 36\pi^2 \times 10^9}{10 \times 4\pi \times 10^{-7}} = \frac{81 \times 10^9 \times 10^7}{10}$$

$$\omega^2 = \frac{81}{10} \times 10^{16} = 8.1 \times 10^{16}$$

$$\boxed{\omega = 2.846 \times 10^8 \text{ rad/sec}}$$

Substitute w in eq (2)

$$E = -\frac{6}{5w_{EO}} \cos(wt - 3y) ax$$

$$E = -476.8 \cos(2.846 \times 10^8 t - 3y) ax \text{ V/m}$$

## Electric Boundary conditions:

When an electric field passes from one medium to other medium, it is important to study the conditions at the boundary between the two media.

Def: The conditions existing at the boundary of the two media when field passes from one medium to other medium are called boundary conditions.

→ Depending upon the nature of the media, there are two situations of the boundary conditions.

(1) Boundary b/w two perfect dielectrics

(2) Boundary b/w conductor & dielectric (3) conductor & free space.

→ For studying the boundary conditions, the Maxwell's equations for electrostatics are required.

$$\oint \mathbf{E} \cdot d\mathbf{l} = 0 \quad \text{and} \quad \oint_S \mathbf{D} \cdot d\mathbf{s} = Q.$$

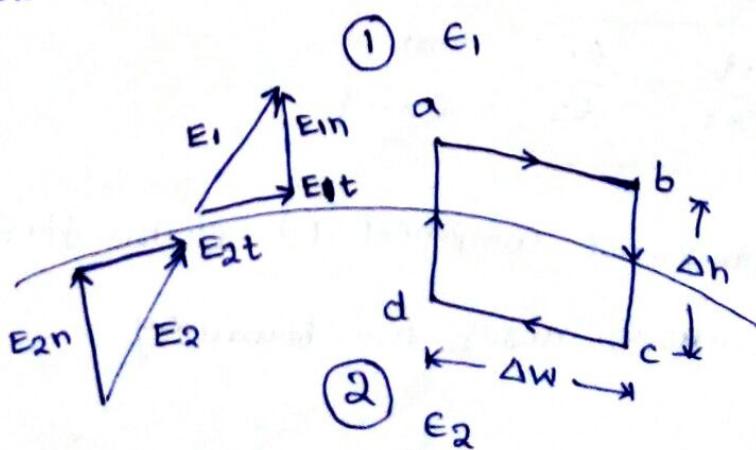
Similarly  $\mathbf{E}$  &  $\mathbf{D}$  are decomposed into two components.

$$\begin{aligned} \mathbf{E} &= E_t + E_n \\ \mathbf{D} &= D_t + D_n \end{aligned}$$

$t \rightarrow$  tangential to the boundary  
 $n \rightarrow$  normal to the boundary.

### (1) Boundary conditions b/w two perfect Dielectrics :

let us consider one dielectric has permittivity  $\epsilon_1$  while other has permittivity  $\epsilon_2$ . The interface is shown in below fig.



### E<sub>t</sub> at Boundary.

Consider a closed path abcd a rectangular in shape having elementary height  $\Delta h$  & elementary width  $\Delta w$ , as shown in above fig. Let us evaluate integral of  $E \cdot d\ell$  along this path in clockwise direction as a-b-c-d-a.

$$\oint E \cdot d\ell = 0$$

$$\therefore \int_a^b E \cdot d\ell + \int_b^c E \cdot d\ell + \int_c^d E \cdot d\ell + \int_d^a E \cdot d\ell = 0$$

Now the rectangle to be reduced at the surface to analyse the boundary conditions. Then  $\Delta h \rightarrow 0$ .

As  $\Delta h \rightarrow 0$ ,  $\int_b^c$  &  $\int_d^a$  becomes zero.

therefore  $\int_a^b E \cdot d\ell + \int_c^d E \cdot d\ell = 0$

$$E_1 t \Delta w + (-E_2 t \Delta w) = 0$$

$$E_1 t \Delta w = E_2 t \Delta w$$

$$\boxed{E_1 t = E_2 t}$$

thus the tangential components of electric field-intensity at the boundary in both the dielectrics remain same i.e. electric field intensity is continuous across the boundary.

→ The relation b/w  $D$  &  $E$  is  $D = \epsilon E \Rightarrow E = \frac{D}{\epsilon}$ .

$$\therefore \frac{D_1 t}{\epsilon_1} = \frac{D_2 t}{\epsilon_2}$$

$$\boxed{\frac{D_1 t}{D_2 t} = \frac{\epsilon_1}{\epsilon_2} = \frac{\epsilon \sigma_1}{\epsilon \sigma_2}}$$

thus the tangential component of electric flux density  $D$  is discontinuous across the boundary.

## D<sub>n</sub> at Boundary

2

To find normal components,

let us, use Gauss's law.

→ consider a Gaussian Surface of right circular cylinder as shown in fig.

According to Gauss's law,  $\oint_S D \cdot dS = Q$ .

$$\therefore \int_{\text{top}} D \cdot dS + \int_{\text{bottom}} D \cdot dS + \int_{\text{lateral}} D \cdot dS = Q$$

Now the cylinder to be reduced at the surface to analyse the boundary conditions. Then  $\Delta h \rightarrow 0$

As  $\Delta h \rightarrow 0$ ,  $\int_{\text{lateral}} D \cdot dS$  becomes zero

therefore  $\int_{\text{top}} D \cdot dS + \int_{\text{bottom}} D \cdot dS = Q$

$$\Delta S D_{in} - D_{2n} \Delta S = P_s \Delta S$$

$$D_{in} - D_{2n} = P_s$$

$$D_{in} - D_{2n} = 0$$

$$\therefore D_{in} = D_{2n}$$

Lateral Surface  $2\pi r \Delta h$

$$\rightarrow P_s = \frac{dQ}{dS} \Rightarrow dQ = P_s dS$$

$$Q = \int P_s dS = P_s \int dS$$

$$Q = P_s \Delta S$$

→ In a perfect dielectric  $P_s = 0$

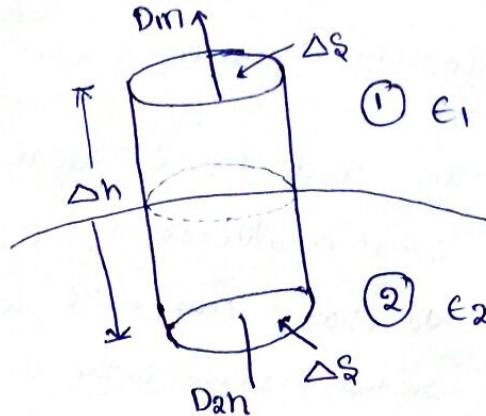
Thus normal component of electric flux density  $D$  is continuous across the boundary.

→ Relation b/w  $D \& E = D = \epsilon_0 E \Rightarrow$

$$E_{in} \epsilon_1 = E_{2n} \epsilon_2$$

$$\frac{E_{in}}{E_{2n}} = \frac{\epsilon_2}{\epsilon_1} = \frac{\epsilon_0 \epsilon_2}{\epsilon_0 \epsilon_1}$$

Thus normal component of electric field intensity  $E$  is discontinuous across the boundary.



## (2) Boundary Conditions b/w Conductor & Dielectric:

$$I = \sigma E$$

$$\sigma = \frac{I}{E}$$

The conductor is ideal having infinite conductivity.

For ideal conductor (i)  $E = 0$ , hence  $D = \epsilon E = 0$ . (inside the conductor)

(ii) No charge can exist within a conductor. The charge appears on the surface in the form of surface charge density.

(iii) The charge density within the conductor is zero.

Thus  $E$ ,  $D$  &  $\rho_s$  within the conductor are zero while  $\rho_s$  is exist.

At the Boundary.

Consider a closed path

abcd rectangular in shape

having elementary height  $\Delta h$  &  
elementary width  $\Delta w$  as shown  
in fig.

→ From Maxwell's equation

$$\oint E \cdot dL = 0$$

$$\therefore \int_a^b E \cdot dL + \int_b^c E \cdot dL + \int_c^d E \cdot dL + \int_d^a E \cdot dL = 0$$

$$\int_a^b E \cdot dL + \int_b^2 E \cdot dL + \int_2^c E \cdot dL + \int_c^d E \cdot dL + \int_d^1 E \cdot dL + \int_1^a E \cdot dL = 0$$

→ In a conductor  $E = 0$

Hence  $\int_2^c$ ,  $\int_2^d$  and  $\int_1^a$  becomes zero.

Therefore  $\int_a^b E \cdot dL + \int_b^2 E \cdot dL + \int_1^a E \cdot dL = 0$ .

$$E_{it} \Delta w + E_{in}(\frac{\Delta h}{2}) - E_{in}(\frac{\Delta h}{2}) = 0$$

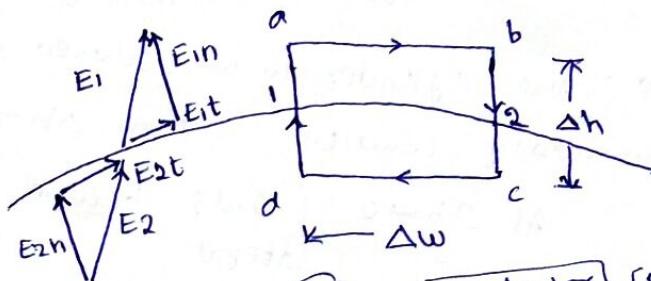
$$E_{it} \Delta w = 0$$

$$E_{it} = 0$$

thus the tangential component of the electric field intensity is zero at the boundary b/w conductor and dielectric.

① Dielectric  $[E = \epsilon_0 \epsilon_r E]$

② Conductor  $[E = 0]$



$$\rightarrow \text{Relation b/w } D \& E \text{ is } D = \epsilon E \Rightarrow E = \frac{D}{\epsilon}.$$

3

$$\frac{D_1 t}{\epsilon_1} = 0 \Rightarrow \boxed{D_1 t = 0}$$

thus the tangential component of electric flux density is zero at the boundary b/w conductor & dielectric.

$D_n$  at the boundary.

To find normal components,

let us use Gauss's Law.

$\rightarrow$  Consider a Gaussian Surface of right circular cylinder as shown in fig.

$\rightarrow$  According to Gauss Law.

$$\oint_S D \cdot dS = Q$$

$$\therefore \int_{\text{top}} D \cdot dS + \int_{\text{bottom}} D \cdot dS + \int_{\text{lateral}} D \cdot dS = Q$$

$\rightarrow$  In a conductor  $D=0$ , Hence  $\int_{\text{bottom}}$  becomes zero.

At the boundary  $\Delta h \rightarrow 0$ , ~~so~~ Hence  $\int_{\text{lateral}}$  becomes zero.

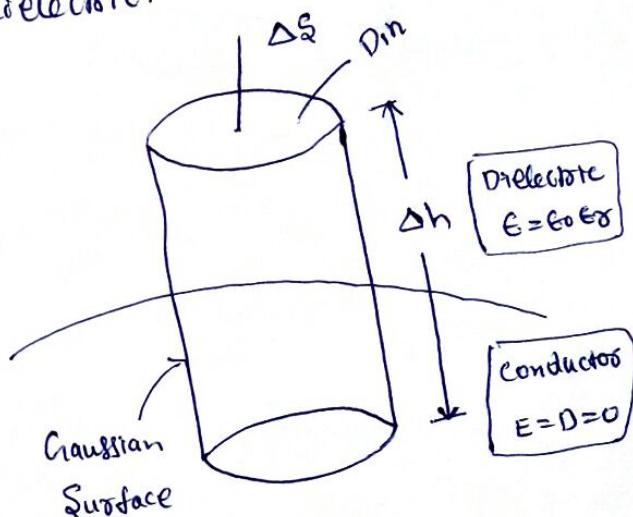
$$\text{And } P_s = \frac{dQ}{dS} \Rightarrow dQ = P_s dS \Rightarrow Q = \int_p P_s dS = P_s \Delta S$$

$$\therefore \int_{\text{top}} D \cdot dS + 0 + 0 = Q$$

$$D_n \Delta S = P_s \Delta S$$

$$\boxed{D_n = P_s}$$

thus normal component of electric flux density  $D$  is equal to the surface charge density.



Relation b/w D & E & O = GE

$$E_{int} = P_S$$

$$E_{int} = \frac{P_S}{\epsilon}$$

## Magnetic Boundary conditions:

The conditions of the magnetic field existing at the boundary of the two media when the magnetic field passes from one medium to other medium are called magnetic boundary conditions.

→ For studying the boundary conditions, the Maxwell's equations for magnetostatics are required.

$$\oint \mathbf{B} \cdot d\mathbf{s} = 0 \quad \text{and} \quad \oint \mathbf{H} \cdot d\mathbf{l} = I$$

### D<sub>n</sub> at Boundary:

To find normal components,

let us use Gauss's law.

→ Consider a Gaussian Surface in the form of right circular cylinder as shown in fig.

→ According to Gauss law  $\oint \mathbf{B} \cdot d\mathbf{s} = 0$

$$\therefore \int_{\text{top}} \mathbf{B} \cdot d\mathbf{s} + \int_{\text{bottom}} \mathbf{B} \cdot d\mathbf{s} + \int_{\text{lateral}} \mathbf{B} \cdot d\mathbf{s} = 0$$

Now the cylinder to be reduced at the surface to analyse the boundary conditions. Then  $\Delta h \rightarrow 0$ ; As  $\Delta h \rightarrow 0$ ,  $\int_{\text{lateral}} \mathbf{B} \cdot d\mathbf{s}$  becomes zero.

$$\text{therefore } \int_{\text{top}} \mathbf{B} \cdot d\mathbf{s} + \int_{\text{bottom}} \mathbf{B} \cdot d\mathbf{s} = 0$$

$$B_1 n \Delta S - B_2 n \Delta S = 0$$

$$B_1 n = B_2 n$$

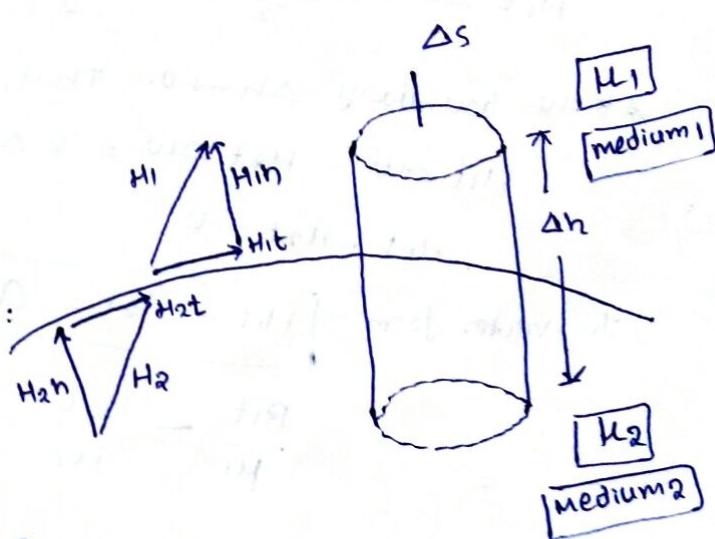
thus normal component of  $\mathbf{B}$  is continuous at the boundary.

→ The relation b/w  $B$  &  $H$  is  $B = \mu H$

$$\mu_1 H_1 n = \mu_2 H_2 n \Rightarrow$$

$$\frac{H_1 n}{H_2 n} = \frac{\mu_2}{\mu_1} = \frac{\mu_2}{\mu_1}$$

thus normal component of  $\mathbf{H}$  is discontinuous at the boundary.



## Et at Boundary

Consider a closed path abcd as shown in fig.

According to Ampere's circ law

$$\oint H \cdot dL = I$$

$$\therefore \int_a^b H \cdot dL + \int_b^c H \cdot dL + \int_c^d H \cdot dL + \int_d^a H \cdot dL = I$$

Assume that  $\kappa$  is the surface current normal to the path.

$$H_1 t \Delta w + H_1 n \frac{\Delta h}{2} + H_2 t \frac{\Delta h}{2} - H_2 n \frac{\Delta h}{2} - H_1 n \frac{\Delta h}{2} = \kappa \Delta w$$

At the boundary  $\Delta h \rightarrow 0$ . Thus,

$$H_1 t \Delta w - H_2 t \Delta w = \kappa \Delta w$$

$$H_1 t - H_2 t = \kappa$$

In vector form

$$H_1 t - H_2 t = \hat{a}_{n12} \times \kappa$$

$$\frac{B_1 t}{\mu_1} - \frac{B_2 t}{\mu_2} = \kappa$$

### Special case:

media are not conductors; so  $\kappa=0$ . Then

$$H_1 t - H_2 t = 0 \Rightarrow H_1 t = H_2 t$$

thus tangential component of  $H$  is continuous at the boundary.

$$\frac{B_1 t}{\mu_1} = \frac{B_2 t}{\mu_2} \Rightarrow \boxed{\frac{B_1 t}{B_2 t} = \frac{\mu_1}{\mu_2} = \frac{\mu_{r1}}{\mu_{r2}}}$$

thus tangential component of  $B$  is discontinuous at the boundary.

